

AMENDMENTS TO THE SPECIFICATION:

Page 1, before line 1, insert:

--Priority is claimed under 35 U.S.C. §119(a) for the filing of Swedish Application No. 0203133-4 on October 22, 2002, and under 35 U.S.C. §119(e) for the filing of U.S. Provisional Application No. 60/477,947 on June 13, 2003.--

Please replace the paragraph beginning on page 1, line 20 and ending on page 1, line 26, with the following amended paragraph:

By using warm compaction, a process where the compaction is performed at an elevated temperature, typically at 120 to 250°C, the density can be increased with about $\pm 0.2 \text{ g/cm}^3$, which results in a considerable improvement of the mechanical properties. A disadvantage is however that the warm compaction method involves additional investment and processing. Other processes, such as double pressing, double sintering, sintering at elevated temperatures etc., may further increase the density. Also these methods will add further production costs hence reducing the overall cost effectiveness.

Please replace the paragraph beginning on page 2, line 19 and ending on page 2, line 22, with the following amended paragraph:

The term "high density" is intended to mean compacts having a density of about at least 7.3 g/cm^3 . "High density" is not an absolute value. A typical achievable density

according to the state of the art for single pressed, single sintered components is about ~~7.1~~ 7.1 g/cm³. By using warm compaction an increase of about ~~0.2~~ 0.2 g/cm³ may be reached.

Please replace the paragraph beginning on page 3, line 21 and ending on page 3, line 27, with the following amended paragraph:

The influence of particle size distribution and the influence of particle shape on the compaction properties and properties of the compacted body have been subjected to intense studies. Thus the ~~US patent 5,594,186~~ U.S. Patent No. 5,594,186 reveals a method of producing PM components with a density higher than 95% of theoretical density by utilising substantially linear, acicular metal particles having a triangular cross section. Powders having coarse particles are also used for the manufacture of soft magnetic components as disclosed in e.g., ~~the US patent 6 309 748 and 4 190 441~~ U.S. Patent Nos. 6,309,748 and 4,190,441.

Please replace the paragraph beginning on page 4, line 12 and ending on page 4, line 22, with the following amended paragraph:

In this context it may be mentioned that ~~the US patents 5766304, 5989304, 6139600, 6235076 and 6451082~~ U.S. Patent Nos. 5,766,304; 5,989,304; 6,139,600; 6,235,076; and 6,451,082 disclose that very small amounts, i.e. 0.05 or less % by weight of the total composition to be compacted, of organoalkoxysilanes may be used as surface treating agents for iron or iron-based powder in combination with lubricating agents. In the

four first ~~US~~ U.S. patents the following silane compounds are tested:

γ -methacryloxypropyl trimethoxy silane, γ -glycidoxypopyl trimethoxy silane, N-beta.(aminoethyl)- γ -trimethoxy silane, methyl trimethoxy silane, fenyl trimethoxy silane and diphenyl dimethoxy silane). In the ~~US patent 6451082~~ U.S. Patent No. 6,451,082, the compounds triphenylmethoxysilane, diphenyldimethoxysilane, phenyltrimethoxysilane, isobutyltrimethoxysilane, and methyltriethoxysilane have been used. The type of organosilanes with lubricating effect used according to the present invention are thus neither mentioned nor tested.

Please replace the paragraph beginning on page 5, line 6 and ending on page 5, line 9, with the following amended paragraph:

For some applications it may be necessary to add minor amounts of graphite to the powder mixture to be compacted. Thus graphite in amounts between 0.1 - 1.0, preferably 0.2 - ~~1.0~~ 1.0 and most preferably 0.3 - 0.8% by weight of the total mixture to be compacted should be added before the compaction.

Please replace the table on page 9, with the following amended table:

	Pow- der C	Pow- der C	Pow- der C	Pow- der C	Pow- der S	Pow- der C	Pow- der S	Pow- der C	Pow- der S	Pow- der S
Silane	0,03% <u>0.03%</u>	0,05% <u>0.05%</u>	0,1% <u>0.1%</u>	0,2% <u>0.2%</u>	0,2% <u>0.2%</u>	0,3% <u>0.3%</u>	0,3% <u>0.3%</u>	0,4% <u>0.4%</u>	0,4% <u>0.4%</u>	0,5% <u>0.5%</u>
E	Sei- zure	62 kN OK 7,67 <u>7.67</u> g/cm ³	39 kN OK 7,66 <u>7.66</u> g/cm ³	39 kN OK 7,67 <u>7.67</u> g/cm ³	65 kN OK 7,61 <u>7.61</u> g/cm ³	33 kN OK 7,66 <u>7.66</u> g/cm ³	38 kN OK 7,63 <u>7.63</u> g/cm ³			
D			48 kN OK 7,65 <u>7.65</u> g/cm ³	46 kN OK 7,66 <u>7.66</u> g/cm ³	47 kN OK 7,63 <u>7.63</u> g/cm ³	36 kN OK 7,64 <u>7.64</u> g/cm ³	34 kN OK 7,62 <u>7.62</u> g/cm ³			29 kN OK 7,56 <u>7.56</u> g/cm ³
C						Sei- zure		37 kN OK 7,60 <u>7.60</u> g/cm ³	66 kN OK 7,60 <u>7.60</u> g/cm ³	97 kN OK 7,53 <u>7.53</u> g/cm ³
B						Sei- zure				
A						Sei- zure				

* unstable value

(OK = fine/satisfactory surface finish;

seizure-seized component surface with scoring marks)

Please replace the paragraph beginning on page 10, line 1 and ending on page 10, line 6, with the following amended paragraph:

As can be seen from the table a chain length of at least 8 atoms in the alkylene chain is needed in order to successfully eject the component for an added amount of silanes of ~~0,05-0,5~~ 0.05-0.5%. Added amounts above ~~0,5~~ 0.5% is believed to be of less interest as the density of the green component will be negatively influenced. The table also shows that when the silane content is less than ~~0,05~~ 0.05% ejection without damaging the component and the surface of the die is not possible for silanes with a chain length of 30 atoms.